# RATE DETERMINING PROCESSES OF SEA ICE GROWTH

by

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### ABSTRACT

We have derived an analytical expression for the growth rate of sea ice by taking account of the processes relevant to the growth, eg heat conduction, diffusion of salt molecules, radiation, sensible heat transport, evaporation and so on. We discuss the role of each process as rate determining processes under various environmental conditions. It is shown that because of coupling of salt diffusion and heat conduction, the growth rate feeds back to the heat flux  $Q_w$  from water to ice which controls the growth rate and that  $Q_w$  decreases with the thickness I of sea ice, even if the environmental conditions are kept constant.

#### INTRODUCTION

Growth of sea ice is the growth of ice crystals from the melt which contains salt of high concentration. The following processes are relevent to the growth: (i) Conduction process through ice of the latent heat of freezing generated at the growing ice/water interface and of the heat coming from water to ice, (ii) Diffusion process of salt molecules rejected by ice at the interface, and (iii) Incoming and outgoing processes of various heats at the upper ice surface, eg the radiation heat, the sensible heat, the latent heat of sublimation, and the conductive heat through ice. These processes are coupled to each other in a very complicated manner.

The purposes of this paper are firstly to derive an analytical expression for the growth rate of sea ice from which we can physically picture the phenomenon by using a simple model (Figure 1) and taking into account the above processes, and secondly to discuss the role of each process as rate determining process under various environmental conditions.

## A MODEL OF GROWING SEA ICE

Let us pursue the growth of sea ice using a simple model illustrated in Figure 1. The model is based on the following assumptions:



Fig.1. Schematic illustration of a model of growing sea ice. Temperature profile (b) and salinity profile (c).

1) Atmosphere, ice and water are horizontally homogeneous so that temperature T and salinity S depend on only vertical direction z (Figure 1).

2) The temperature profile in ice is governed by the solution of the equation of heat conduction under steady state conditions, i e

$$\frac{\partial T}{\partial t} = \frac{\kappa_i}{c\rho} \frac{\partial^2 T}{\partial_z^2} = 0, \qquad (1)$$

where  $\kappa_i$  is the thermal conductivity,  $\rho$  the density and c the specific heat of sea ice. Therefore, T is linearly proportional to z:

$$\Gamma = T_s + \frac{T_{int} - T_s}{I} z \quad (0 \le z \le I), \qquad (2)$$

where  $T_s$  is the temperature of the upper surface of ice (z = 0),  $T_{int}$  the temperature of the ice/water interface (z = 1), ie the lower surface of ice, and I the thickness of ice. However, the change in temperature at a fixed position in ice is taken into account through an increase in I with time. Such a solution is called a quasi-steady state solution. In the Equation 1, internal heating due to incoming short-wave radition is neglected. The conductive heat flux through ice is given by

$$Q_i = \kappa_i \frac{T_{int} - T_s}{I} .$$
 (3)

3) A diffusion boundary layer with a thickness  $\delta_d$  is formed in the seawater near the lower surface of ice (Figure 1a and 1c). Since only a part of the salt molecules in water can be incorporated into ice, the remainder is rejected at the growing lower surface of ice and the salinity  $S_{int}$  in water adjacent to the lower surface (z = I) becomes larger than the salinity  $S_w$  of water at Z >> I. The rejected salt molecules are carried away by diffusion in the boundary layer with a flux

$$J_{d} = D \frac{S_{int} - S_{w}}{\delta_{d}} , \qquad (4)$$

where D is the diffusion constant of salt molecules in water.

4) The salinity  $S_i$  of ice determined by incorporation kinetics at z = I is proportional to  $S_{int}$ .

$$S_i = k^* S_{int}$$
 (5)

where k\* is the so-called distribution coefficient at the cellular ice/water interface (Weeks and Lofgren 1967).

5) The temperature  $T_{int}$  at z = I is equal to the freezing temperature which is determined by the salinity  $S_{int}$ :

$$T_{int} = 273 - \alpha S_{int} , \qquad (6)$$

where  $\alpha$  is the slope of the liquidus line of the phase diagram of a water-salt system. Therefore,  $T_{int}$  is lower than  $T_w$  by

$$T_w - T_{int} = \alpha(S_{int} - S_w)$$
 (7)

6) A thermal boundary layer with a thickness  $\delta_t$  exists in water near the lower surface of ice (Figure 1a and 1b). Therefore, the conductive heat flux from water to ice is given by

$$Q_{w} = \kappa_{w} \frac{T_{w} - T_{int}}{\delta_{t}} , \qquad (8)$$

$$Q_{w} = \kappa_{w} \frac{\alpha(S_{int} - S_{w})}{s_{t}}, \qquad (8)'$$

where  $\kappa_w$  is the thermal conductivity of seawater.

(

7) There are several incoming and outgoing heat fluxes at the upper surface (z = 0) of ice. Incoming fluxes include long-wave radiation Qin from the atmosphere, short-wave radiation  $Q_s^{in}$  and conductive heat  $Q_i$  through the ice towards the upper surface. Outgoing fluxes consist of long-wave radiation  $Q_s^{out}$ , sensible heat  $Q_{sen}$  and latent heat of sublimation Q<sub>sub</sub>.

$$Q_{I}^{out} \text{ is given by}$$

$$Q_{I}^{out} = \epsilon \sigma T_{s}^{4}$$

$$Q_{I}^{out} = \epsilon \sigma T_{a}^{4} + 4\epsilon \sigma T_{a}^{3} (T_{s} - T_{a}), \quad (9)$$

€ is the long-wave emmisivity, o the Stefan-Boltzmann constant and T<sub>a</sub> the temperature of the atmosphere.

 $Q_{sen}$  in W/m<sup>2</sup> is expressed as

$$Q_{sen} = 3.5 U_a (T_s - T_a)$$
, (10)

where U<sub>s</sub> is the wind velocity in m/s (Kuz'min 1972).

Q<sub>sub</sub> is given by

$$Q_{sub} = 1.64 \times 10^{-11} L_{s} \rho U_{a} [p_{e}(T_{s}) - sp_{e}(T_{a})]$$
 (11)

 $Q_{sub} \approx 1.64 \times 10^{-11} L_s \rho U_a [(1-s)p_e(T_a) +$ 

+ 
$$\left[\frac{\partial p_e}{\partial T}\right]_{T_a} \left[T_s - T_a\right]$$
, (11)'

where  $L_{g\rho}$  is the latent heat of sublimation in  $J/m^3$ , s the humidity,  $\mathbf{p}_{c}(T)$  the saturation vapour pressure of ice at T in Pa and  $(\partial \mathbf{p}_{e}/\partial T)_{T}$  the temperature coefficient of the saturation vapour pressure at T given by the Clausius-Clapeyron equation. Equation 11 was derived from the empirical relation obtained by Ono and others (1980).

DETERMINATION OF THE GROWTH OF SEA ICE Heat balance at the lower surface of ice

The process which directly controls the growth rate V of sea ice is the conduction process of the latent heat of freezing. From the heat budget equation at z = I, we obtain an expression

$$V = \frac{1}{L_{f}\rho} \left[ \kappa_{i} \frac{T_{int} - T_{s}}{I} - \kappa_{w} \frac{T_{w} - T_{int}}{\delta_{t}} \right], \quad (12)$$

where  $L_{f\rho}$  is the latent heat of freezing in J/m<sup>3</sup>. Now determine  $T_{int}$  and  $T_{s}$  which are closely tied to the processes (i) to (iii) mentioned above.

Equilibrium condition for  $T_{int}$ As shown in Equation 6,  $T_{int}$  is assumed to be equal to the equilibrium freezing temperature corresponding to the salinity  $\hat{S}_{int}$  which is determined by the following mass conservation conditions of salt molecules at z = I.

Mass balance of salt molecules at the lower surface of ice Since only a portion of the salt molecules in water is incorporated into ice at z = I (see Equation 5), the salt molecules are rejected there by amount of  $V(S_{int} - S_i) = V(1 - k^*)S_{int}$  per unit time and unit area. The quantity should be equal to the diffusion flux  $J_d$  given by Equation 4 under steady state conditions:

$$V (1 - k^*)S_{int} = D \frac{S_{int} - S_w}{s_d}$$
 (13)

Therefore, we obtain a relation between S<sub>int</sub> and V

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(17)

$$S_{int} = S_{\mathbf{w}} \begin{bmatrix} 1 + \delta_d (1 - k^*) V / D \end{bmatrix}.$$
(14)

Heat balance at the upper surface of ice

The temperature  $T_a$  is determined by the balance equation of the heat fluxes at z = 0 mentioned in section 2:

$$\begin{aligned} Q_{I}^{in} + (1-\partial) Q_{s}^{in} + \kappa_{i} \frac{T_{int} - T_{s}}{I} - \epsilon \sigma \left[T_{a}^{4} + 4T_{a}^{3}(T_{s} - T_{a})\right] - \\ &- 3.5U_{a}(T_{s} - T_{a}) - 1.6 \times 10^{-11}L_{s}\rho U_{a}\left[(1-s)p_{e}(T_{a}) + \left(\frac{\partial p_{e}}{\partial T}\right)_{T_{a}}(T_{s} - T_{a})\right] = 0 , \end{aligned}$$

$$(15)$$

where  $\partial$  is the surface albedo. From this equation, we obtain

$$T_{s} = \frac{T_{a} - B/A + (\kappa_{i}/IA)T_{int}}{1 + \kappa_{i}/IA} , \qquad (16)$$

where

$$A = 4\epsilon\sigma T_a^3 + 3.5U_a + 1.6x10^{-11}L_{g}\rho U_a(\partial p_e/\partial T)_{T_a}$$

and

$$B = \epsilon \sigma T_{a}^{4} + 1.6 \times 10^{-11} L_{s} \rho U_{a} (1-s) p_{e} (T_{a}) - [Q_{g}^{in} + (1 - \vartheta) Q_{s}^{in}].$$
(18)

A = 23.4 W/m<sup>2</sup>K and B = 60.7 W/m<sup>2</sup>, if we assign T<sub>a</sub> = 253 K,  $\epsilon = 1$ ,  $\sigma = 5.67 \times 10^{-8}$  W/m<sup>2</sup>K<sup>4</sup>, U<sub>a</sub> = 5 m/s, L<sub>a</sub>  $\rho = 2.6 \times 10^{9}$  J/m<sup>3</sup>,  $(\partial p_e / \partial T)_T = 10.4$  Pa/K,  $p_e(T_a) = 1.03 \times 10^{2^{9}}$  Pa,

s = 0.8,  $Q_g^{in} = 1.76 \times 10^2 \text{ W/m}^2$  and  $Q_s^{in} = 0$ . From Equation 16 one can see that  $T_g = T_a$  for A→∞ and  $T_g = T_{int}$  for  $\kappa_i \rightarrow \infty$ . These results are plausible. It should be noted that  $T_{int}$  and  $T_g$  which control the growth rate V (Equation 12) themselves depend on V (see Equations 6, 14 and 16).

Growth rate

By solving Equations 12, 6, 14 16 and self-consistently, we can obtain an expression for the growth rate V as a function of temperature  $T_a$  of the atmosphere and T, of sea water:

$$V = \zeta \frac{\kappa_i}{L_f \rho} \frac{T_w - T_s}{I}, \qquad (19)$$

where

$$T_w = 273 - \alpha S_w$$
, (20)

 $T'_{z}$  is the temperature at the upper surface of ice (z = 0) when  $T_{int} = T_w$  in Equation 16. ie

$$T_{s}^{\prime} = [T_{a} - B/A + (\kappa_{i}/IA) T_{w}]/(1 + \kappa_{i}/IA),$$
 (16)

and

$$\zeta = 1 / \left[ 1 + \frac{\alpha S_{w}(1-k^{*}) \delta_{d}}{L_{f} \rho D} \left\{ \frac{\kappa_{i}}{I} \left[ 1 - \frac{\kappa_{i}/IA}{1-\kappa_{i}/IA} \right] + \frac{\kappa_{w}}{\delta_{t}} \right\} \right].$$
(21)

The obtained growth rate includes the physical quantities relevant to the processes of freezing, conduction of the latent heat of freezing, incorporation of salt into ice, diffusion of salt molecules, incoming and outgoing radiation, transport of sensible heat and latent heat of sublimation as described above.

# DISCUSSION

Growth rate

Using Equations 19, 20, 16' and 21, let us discuss the influence of the environmental conditions on the growth rate of sea ice.

In the most extreme case that  $S_w = 0$  and  $A \rightarrow \infty$ ,  $T_{int} = T_w = 273$  K,  $T_s = T_a$  and  $\zeta = 1$ . Therefore, we obtain the simplest Stefan equation  $V^{(0)}$  from Equation 19:

$$V^{(0)} = \frac{\kappa_i}{L_f \rho} \frac{273 - T_a}{I} .$$
 (19)

If  $S_w > 0$  and  $D \rightarrow \infty$ ,  $S_{int}$  is equal to  $S_w$  because of infinite rate of diffusion of rejected salt molecules, then  $T_{int} = T_w$  and  $\zeta = 1$ . In this case, the growth rate is expressed as

$$V^{(1)} = \frac{\kappa_{\rm i}}{L_{\rm f}\rho} \frac{T_{\rm w} - T_{\rm s}'}{\rm I} .$$
 (19)''

In the general case that  $S_w > 0$  and D is finite,  $S_{int}$ > because of finite rate of diffusion of salt molecules, S. consequently  $T_{int} < T_w$  and  $\zeta < 1$ . Therefore, the growth rate V in the general case given by Equation 19 is smaller than  $V^{(1)}$  by a factor of  $\zeta$ . It should be noted that  $1/\zeta$ corresponds to the interface resistance to the growth due to the coupling processes of material and heat transports in the diffusion and thermal boundary layers (Figure 1).

With increasing  $S_w$  the growth rate decreases because of a decrease in  $V^{(1)}$  and  $\zeta$  in this model. The first effect is due to a decrease in  $T_w$  with  $S_w$ . On the other hand, the second effect is rather complicated. Since an increase in  $S_w$ makes the diffusion of salt molecules slower (the right side of Equation 13) and consequently raises  $S_{int}$  (Equation 14),  $T_{int}$  falls with  $S_w$  (Equation 6). Therefore, V decreases with  $T_{int}$  falls with  $S_w$  (Equation 6). Therefore, V decreases with  $S_w$  (Equation 12). A decrease in  $\zeta$  with  $S_w$  represents this effect.

In this paper, we assume that the thickness  $\delta_d$  of diffusion boundary layer is given. The value of  $\delta_d/D$  reported by Weeks and Lofgren (1967) is  $5.09 \times 10^5$  s/m and that by Nakawo and Sinha (1981) is  $4.2 \times 10^6$  s/m. If D is assumed to be 1 x  $10^{-9}$  m<sup>2</sup>/s,  $\delta_d = 0.51$  mm in the former case and  $\delta_d = 4.2$  mm in the latter case. The thickness  $\delta_d$  is avanted to decrease with flow value in the latter set. thickness  $\delta_d$  is expected to decrease with flow velocity  $U_w$  of water, since the thickness of velocity boundary layer decreases with  $U_w$ . A decrease in  $\delta_d$  leads to an increase in  $\zeta$  or V because of faster diffusion of salt molecules. However, the influence of  $U_w$  on V through the thickness  $\delta_t$  of thermal boundary layer is different. With increasing  $U_w$ ,  $\delta_t$  may also decrease. And  $\zeta$  decreases with decreasing  $\delta_t$  (Equation 21), since the heat flux  $Q_w$  from water to ice increases with decreasing  $\delta_t$  (the second term of the right side in Equation 12).

The dependence of the growth rate on the thickness I for calculation are as follows:  $T_a = 253 \text{ K}$ ,  $\kappa_i = 2.26 \text{ W/m}$ K,  $\kappa_w = 0.52 \text{ W/m}$  K,  $\alpha = 0.055 \text{ K/}^{\circ}/\infty$ ,  $S_w = 32.9^{\circ}/\infty$ ,  $L_f \rho = 3.08 \times 10^8 \text{ J/m}^3$ ,  $k^* = 0.12$ ,  $\epsilon_d/D = 4.2 \times 10^6 \text{ s/m}$ ,  $\delta_t = 2 \times 10^{-2} \text{m}$ ,  $A = 23.4 \text{ W/m}^2$  K and  $B = 60.7 \text{ W/m}^2$ . With increasing I, V<sup>(1)</sup> decreases because of a decrease in conductive heat flux in ice. On the other hand, 5 slightly increases with I, since the flux of rejected salt moelcules decreases with decreasing growth rate (see the left side of Equation 13). However, this is a secondary effect, so that V =  $\zeta V^{(1)}$  decreases with I.

Effective distribution coefficient  $k_{eff}$ From Equations 5 and 14, we obtain the so-called effective distribution coefficient  $k_{eff} = S_i/S_w$  of salt molecules.

$$k_{aff} = k^* \left[ 1 + \delta_d (1 - k^*) V / D \right], \tag{22}$$

where V is given by Equation 19. The salinity  $S_i$  in ice is expected to decrease with z (Figure 1c), since the growth rate V in Equation 22 decreases with I. The Equation 22 coincides with the expression for keff derived by Weeks and Lofgren (1967), if  $\delta_d V/D \ll 1$ .

Heat flux  $Q_w$  from water to ice Using Equations 8' and 14, the heat flux  $Q_w$ from water to ice is given by

$$Q_w = \kappa_w (1 - k^*) \alpha S_w (\delta_d / \delta_t) V/D. \qquad (8)''$$

This equation means that the growth rate V feeds back to the heat flux  $Q_w$  which controls V because of coupling of salt diffusion in the diffusion boundary layer and heat conduction in the thermal boundary layer.

TABLE 1. THE DEPENDENCE ON THE THICKNESS I OF SEA ICE OF THE GROWTH RATE V AND THE HEAT FLUX Qw FROM WATER TO ICE.

I [m]	0.1	0.5	1.0
V <sup>(1)</sup> [m/s]	7.7 x 10 <sup>-7</sup>	2.5 x 10 <sup>-7</sup>	1.4 x 10 <sup>-7</sup>
ζ	0.56	0.62	0.63
$V = \zeta V^{(1)} [m/s]$	4.3 x 10 <sup>-7</sup>	1.6 x 10 <sup>-7</sup>	8.7 x 10 <sup>-8</sup>
$Q_w [W/m^2]$	71.4	26.1	14.4

As shown in Table 1, Q<sub>w</sub> decreases with the thickness I of sea ice, even if the environmental conditions are kept constant. An increase in I leads to a decrease in  $S_{\rm int}$  (Equation 14), since V decreases with I. Therefore,  $Q_{\rm w}$  falls with I (Equations 8' and 14). On calculation, we assumed  $\delta_d/\delta_t = 0.2$  and  $D = 1 \times 10^{-9} \text{ m}^2/\text{s}.$ 

ACKNOWLEDGEMENT

The author is indebted to Professor N Ono and Dr N Ishikawa for helpful discussions.

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