Use of ice-sheet normal modes for initialization and modelling small changes

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ABSTRACT. Linearizations about two horizontal-dimensional ice sheets are proposed as methods of generating normal mode initializations for ice-sheet models and for computing the short-term response. Linearized models can be generated directly from balance-flux calculations without the need for tuning the rate factor.

A linearized model is compared with the Eismint Benchmark, and the normal modes for two coarse Antarctic digital elevation models are computed and compared. Volumetric relaxation spectra are presented. The slowest mode has a time constant comparable to that computed from scale theory.

INTRODUCTION

This paper is concerned with linearization techniques as a way of estimating the glaciological response to changes in the accumulation rate on ice sheets. That is, changes in the accumulation rate result in changes in ice-sheet geometry, which in turn produce changes in the movement of the ice. Linearized methods have, of course, some disadvantages in modelling the non-linear evolution equations for ice sheets, but also have advantages in that the model does not require specification of the rate factor in the viscous law. In this sense, the model is closer to the data than "matched" nonlinear models. Linearization techniques have previously been applied to modern ice sheets (e.g. Oerlemans, 1981; Hindmarsh, 1992; Drewry and Morris, 1992; Van der Veen, 1993), but these have only been of ordinary differential equations (zero-dimensional (0-D)models). This paper presents the first computations of the normal modes of an observed ice sheet.

The disadvantages of this method relate principally to an inability to describe changes in ice-stream flow, which is expected to be non-linear. The disadvantage is more apparent than real, as research methods remain far from creating adequate models of basal and lateral processes in ice streams, and models of ice streams, incorporating what are believed to be the relevant dynamical features, can only provide conjectural prognoses.

The advantages of linearized techniques relate to ease of use for non-glaciologists, and the fact that no model tuning is necessary. That is, in non-linear models (e.g. Huybrechts, 1992) the accumulation rate and the viscous properties are parameterized and tuned in order to obtain a good fit between observed and computed heights. This was an appropriate response a few years ago, but the progress of satellite altimetry since then (Bamber and Huybrechts, 1996) has made ice-sheet elevation the most accurately known of all the ice-sheet descriptors. Linearization methods permit prognostic calculations to be made without knowing the rate factor, as the rate equation stems ultimately from the mass accumulation. Thus, no tuning is necessary and computations of ice-sheet geometry evolution can be compared directly with observations.

Moreover, a practical consequence is that no estimate is required of slow changes in response to, for example, the end of the Last Ice Age before the response to *changes* in forcing can be estimated. One aim of the work described here is the production of ice-sheet models describing a short-term response that can be used in models of other parts of the climate system.

It should be emphasized that linearized models are rational approximations — that is, they come equipped with their own error bars. For small perturbations, linearized methods are accurate and the order of magnitude of the error term can be computed.

The paper will discuss issues of normal mode initialization and spatial filtering of data. The non-linear ice-sheet equations and their linearizations in two horizontal dimensions (2HD), are reviewed and compared to results from the non-linear Eismint Benchmark (Huybrechts and others, 1996). Finally, the modes of a real 2HD ice sheet (the Antarctic ice sheet) are computed.

NORMAL MODE INITIALIZATIONS OF ICE SHEETS

Normal modes are the eigenfunctions and eigenvalues that ensue from setting up a linear(ized) model and solving a related eigenvalue problem. The "normal" pertains to the canonical nature of these modes. Each mode has an associated *e*-folding time constant, and the spatial structure of each mode is different. Essentially, shorter spatial-length scales are expected to relax faster (have a shorter *e*-folding time constant).

Normal modes are widely used in geophysics and geophysical fluid dynamics. Despite being a classical technique, they have not been used widely in glaciology. An important use in meteorology has been the filtering of meteorological data in order to initialize models with data that do not excite

non-physical numerical modes.

As explained above, ice-sheet-model geometry, when compared to real data, represents a trade-off between the tuning of the rate factor and the parameterization of the accumulation-rate distribution. An obvious issue is whether normal mode techniques can be exploited to initialize icesheet models. In particular, the advent of satellite altimetry has produced very accurate elevation data that need to be included in ice-sheet models if dynamics are to be inferred from observations.

When observed elevations are used in non-linear icesheet models, it is found that smaller-scale structure is relaxed out quickly, sometimes causing numerical problems (Oerlemans and Van der Veen, 1984). Current observations of basal topography are nowhere near the same plan-view resolution, meaning that errors in the thickness cause computed and spurious ice-flow anomalies, resulting in the numerical smoothing described above.

An obvious question is whether normal-mode initialization techniques can be used in some form in ice-sheet modelling, with the specific objective of ensuring that observations are used as an initial state, rather than some trade-off between ignorance of accumulation, rate factor, icc-sheet thickness and the need to maintain numerical stability.

Because the ice-sheet equation represents an initial value problem, any measured data are physically consistent. Anomalous roughness and topographic sinks (e.g. the Vostok depression) could simply be relaxing out. Under an assumption of steady state, the origin of many features becomes more problematical, but can still, in principle, be explained by local variations in the poorly known basal topography or, in a more contrived way, by local variations in the rate factors for internal deformation or for sliding. Topographic depressions can arise as a result of locally enhanced basal melting, or may conceivably occur as a result of "Stokes effects", where, for example, small-scale variations in the basal topography result in local failure of the shallow-ice approximation (e.g. Jóhannesson, 1992).

Small-scale (wavelength of a few gridcells) surface roughness, that is not reflected in causatory variation in the rate factor or the basal topography, is relaxed out by the action of non-linear solutions. Balance-flux calculations and ensuing linearizations are not affected by this problem provided topographic depressions are dealt with by setting basal melting to be larger than the accumulation.

Such noisy data can be dealt with in several ways when initializing models:

- (a) Accept the data as a valid zeroth-order approximation and compute a set of eigenfunctions and eigenvalues. It could transpire that even the low wave-number eigenfunctions are noisy.
- (b) Smooth heuristically and compute the normal modes.
- (c) Select a smooth zeroth-order solution on an error minimization criterion and compute the normal modes (Hindmarsh, in press).

In the latter two cases there will be a residual between the zeroth-order solution and the data. This can be reduced by fitting the residual with the normal modes: this is a normal mode initialization as commonly used in other geosciences (e.g. Daley, 1992). The more modes used, the smaller the wavelength of feature that can be modelled. The remaining variation is filtered by using functions that have a close relation to ice-sheet physics rather than by an arbitrary smoothing.

Clearly, if option (a) produces smooth normal modes, then it is the simplest option. Provided sink-holes are eliminated from the observed data, then the computed normal modes do not appear noisy. It is possible that holes could be reconstituted by using the normal modes, but testing the efficacy of this technique is outside the immediate aims of this paper. We shall see that option (a) is possible.

THE ICE-SHEET EQUATION AND ITS LINEARIZA-TIONS

Notation is summarized in Table 1. When considering the mechanics of ice sheets a reduced model is normally used (Hutter, 1983; Morland, 1984; Fowler, 1992), obtained from a scaling of the Stokes equations. The scaling yields simple functional forms for the vertical variation of the stress field and a considerable computational saving. Further manipulation of the reduced model results in the ice-sheet equation:

$$\partial_t H = \nabla \cdot \left(C H^m |\nabla s|^{\nu - 1} \nabla s \right) + a \tag{1}$$

where H(x, y, t) is the thickness of the ice sheet, s(x, y, t) is the upper surface and a is the surface mass-balance exchange. Boundary conditions for this model are:

$$\partial_t H(x, V(x), t) \equiv 0, \tag{2}$$

where y = V(x), the prescribed margin. This corresponds to the Vialov–Nye calving condition, where the ice thickness at the margin is less than the maximum thickness. More advanced models, to be considered in future work, would have non-zero thickness at the grounding line and a moving grounding line. This has already been treated in a linearized fashion for one horizontal dimension (lHD) by Hindmarsh (1996a).

These evolution equations describe the evolution of icesheet thickness where the flow mechanism is *either* internal deformation according to a non-linearly viscous flow law *or*

Table 1. Notation

Variable	Meaning
a	Accumulation rate
C_k	Spatial modes of \bar{s}_k ; Fourier transform of \mathbf{T}
h	Vector over ℓ of H_1
i	Spatial mode index
k	Fourier mode index
l	Point index
\overline{m}	Non-linear diffusion index
q	Flux of ice
s	Ice-sheet elevation
$\bar{s}_{\ell k}; \bar{\mathbf{s}}_k$	Fourier component for point ℓ at frequency k, vector over ℓ
t	Time
(x, y, z)	Space coordinates
C	Rate factor
ε	Eigenfunctions of ${\cal L}$
E	Matrix of eigenvectors
F	Discretization of $\mathcal L$
G	Discretized Green's function corresponding to \mathcal{L}^{-1}
H	Ice-sheet thickness
L	Linear-perturbation operator
т	Vector of mode amplitudes
ν	Flow/sliding-law index
λ	Eigenvalues
Г	Matrix of eigenvalues

sliding according to a Weertman-type law. The analyses carried out in this paper are not limited to these situations.

The quantity C is directly related to either a weighted vertical average rate factor \overline{A}_{d} defined below in Equation (6) of the rate factor A_{d} used in the viscous relationship:

$$E = A_{\rm d} \tau^n \tag{3}$$

where E is a second invariant of the deformation rate and τ is a second invariant of the deviator stress (Glen, 1955) or comes from a sliding relation of the form:

$$u_{\rm b} = A_{\rm s} \tau_{\rm b}^{\,\ell} \tag{4}$$

(Weertman, 1957). We construct the following quantities for use in the general evolution equation:

$$\nu = \begin{cases} n \\ \ell \end{cases}, \quad m = \begin{cases} n+2 \\ \ell+1 \end{cases},$$
$$C = \begin{cases} \frac{2(\rho g)^{\nu}}{\nu+2} \bar{A}_d \\ A_s(\rho g)^{\nu} \end{cases}; \quad \begin{cases} \text{Internal deformation} \\ \text{Sliding.} \end{cases}$$

The derivation of the evolution Equation (1) using the shallow-ice approximation is standard (Hutter, 1983; Morland, 1984; Fowler, 1992). A further standard derivation, which, in the present notation, can be found in Hindmarsh (1996a) yields a formula for the ice flux q:

$$q_{\rm i} = -CH^m |\nabla s|^{\nu-1} \partial_{x_{\rm i}} s \tag{5}$$

where:

$$\bar{A}_{\rm d} = (\nu + 2) \int_0^1 (1 - \zeta)^{\nu + 1} A_{\rm d} d\zeta, \quad \zeta = \frac{z - b}{H} \quad (6)$$

If instead we are dealing with sliding, then:

$$q_{\mathbf{i}} = u_{\mathbf{i}}{}^{\mathbf{b}}H = -CH^{m}|\nabla s|^{\ell-1}\partial_{x_{\mathbf{i}}}s\,,\qquad(7)$$

and use of the continuity equation:

$$\partial_t H + \nabla \cdot \mathbf{q} \big(H, \partial_x H, \partial_y H \big) = a \tag{8}$$

results in the non-linear diffusion type Equation (1). Linearizations are computed by expanding H and a in a series

$$H = H_0 + \mu H_1 + \dots,$$

 $a = a_0 + \mu a_1 + \dots,$

and truncating at first order. The Taylor expansion of q_x , for example, yields:

$$q_x \simeq q_{0x} + \mu q_{1x} \simeq q_{0x} + \\ \mu \left(\frac{\partial q_x}{\partial H} \Big|_{H_0} H_1 + \frac{\partial q_x}{\partial \partial_x H} \Big|_{H_0} \partial_x H_1 + \frac{\partial q_x}{\partial \partial_y H} \Big|_{H_0} \partial_y H_1 \right).$$

Specifically, we can compute:

$$\begin{aligned} \left. \frac{\partial q_i}{\partial H} \right|_{H_0} &= m H_0^{m-1} |\nabla s_0|^{n-1} \partial_{x_i} s_0 = -m q_{i0} / H_0 \\ \left. \frac{\partial q_i}{\partial \lambda_j H} \right|_{H_0} &= H_0^m |\nabla s_0|^{n-3} \left(|\nabla s_0|^2 \delta_{ij} + (n-1) \partial_{x_i} s_0 \partial_{x_j} s_0 \right) \\ &= - q_{i0} \left(\frac{\delta_{ij}}{\partial x_i s_0} + \frac{(n-1) \partial_{x_j} s_0}{|\nabla s_0|^2} \right), \end{aligned}$$

and we can see that the zeroth order and first-order equations are:

$$\nabla \cdot \mathbf{q}_0 = a_0 - \partial_t H_0 \tag{9}$$

$$\partial_t H_1 = -\nabla \cdot \mathbf{q}_1 + a_1,\tag{10}$$

$$q_{i1} = q_{i0} \left\{ \frac{mH_1}{H_0} + \frac{\delta_{ij}\partial_{x_i}s_1}{\partial_{x_i}s_0} + \frac{(\nu - 1)\partial_{x_i}s_0\partial_{x_j}s_0}{\left|\nabla s_0\right|^2} \ \partial_{x_j}s_1 \right\}$$
(11)

Boundary conditions are the crude approximation of fixing the elevation at the margin of the ice sheet. Moving boundaries can be incorporated into linearizations (Hindmarsh, 1996a) but the technical difficulties of extending this approach to two horizontal dimensions mean that it is worth investigating the fixed margin problem first in order to assess the potential of linearization techniques. Ablating margins are not considered in this paper.

The zeroth-order solution can be identified with the long-term trend (e.g. the response to pre-industrial climate conditions) and the first-order solution with the faster response to perturbation. The long-term trend could of course be steady state. If the technique were being applied rigorously time should be expanded in two time-scales, but the complexities of the required notation outweigh the benefits, so the procedure is justified heuristically by saying that the perturbation is expected to grow over time-scales where the zeroth-order solution hardly changes, and a "snap-shot" can be taken of the profile to compute the coefficients in Equation (9)

The curious way of writing the zeroth-order equation is to emphasize that ignorance of accumulation rate and rate of change of surface profile have exactly the same significance. It is assumed that a_1 is known, in the sense that the response to a postulated change in the accumulation rate is being evaluated.

A significant feature of the perturbation equation is the absence of the rate factor in the first-order equation. The time dimension is introduced into the ice-sheet equation by the accumulation rate of snow and through the rate factor. In a strain-rate controlled flow, such as is assumed here, the ice sheet exists to discharge the snowfall, and the time-scales are set by meteorological factors. The ice-sheet geometry adjusts so as to set the rheological time-scale equal to the meteorological time-scale. Where there are internal oscillations in the ice sheet, the fast and slow phases correspond to stress-controlled flows, and the perturbation equation will not apply. In any case, the perturbation equation is a linear equation and cannot have limit cycle solutions such as those described by Payne (1995).

By setting $a_1 = 0$ the linear equation can be put into homogeneous form. A separation of variables technique can be used to generate solutions to the homogeneous form using an eigenvalue expansion, which can subsequently be used to construct solutions to the inhomogeneous form. The theory is reviewed below. In general, the eigenproblem has to be solved numerically. There are potential problems associated with singular behaviour at the divide and margin.

Hindmarsh (1996b, in press) has considered perturbations about the 1HD Vialov–Nye (VN) (Vialov, 1958; Nye, 1959) solution, which is computed by setting $\partial_t H = 0$ and $a = a_{m0}, C = C_{m0}$, both constants, into the plane-flow version of Equation (1) and integrating the resulting ordinary differential equation (ODE). Hindmarsh (in press) treated

the singularities at margin and divide accurately by using Frobenius expansions (see also Fowler, 1992). In the 2HD calculations reported here, Taylor expansions are used at the margin and at the divide. Calculations for 1HD, based on the principles described below for 2HD, show that this makes very little difference to the computed eigenvalues or eigenfunctions. This presumably arises as a result of the robustness of Sturm–Liouville systems to model perturbation (Pryce, 1993). Taylor, rather than Frobenius, expansions are almost universally used in ice-sheet modelling when the non-linear problem is treated.

ZEROTH-ORDER FLUX COMPUTATION CONSIS-TENT WITH FINITE-DIFFERENCE GRIDS

Given that the perturbation procedure will be carried out on a finite-difference grid, it is highly desirable that the zeroth-order fluxes satisfy the conservation equation exactly. For this reason, efficient shooting procedures (Budd and Warner, 1996; Rémy and others, 1996) are not used. The procedure is simply to compute the flux arriving at a gridpoint from x- and y-direction connections, compute the flux out using continuity, and divide it between all the outlet connections (i.e. to points at a lower elevation) in linear proportion to their slopes.

Consider the coefficient $D = CH_0^m |\nabla s_0|^{\nu-1}$. Then, $\mathbf{q} = -D\nabla s_0$. Even though s_0 and H_0 are known, C is not, meaning that D is also unknown. A finite-difference approximation is:

$$q_{i+1/2,j} = D_i \frac{s_{i+1,j} - s_{i,j}}{\Delta_x}$$

for each of the outlet points, where D_i is an unknown. The outlet discharges and D can be solved with the additional equation:

$$\frac{q_{i+1/2,j} - q_{i-1/2,j}}{\Delta_x} + \frac{q_{i,j+1/2} - q_{i,j-1/2}}{\Delta_y} = a_{i,j}.$$

Balance flux calculations have been used by Rémy and others (1996) to solve for the rate factor and thence the basal temperature.

In practice, the grid-centred fluxes are computed by solving a set of linear equations. These satisfy continuity exactly and also return the quantity $D = CH_0^m |\nabla s_0|^{\nu-1}$. While the method is algorithmically different from that of Budd and Warner (1996), the two methods seem to be consistent at $O(\Delta_x)$. The purpose of using a different method is to ensure that the continuity equation is respected exactly at zeroth order on the finite-difference grid used to solve the eigenproblem.

THE EIGENVALUE PROBLEM AND ITS DISCRETI-ZATION

The first-order perturbation Equations (10) and (11) are conveniently written in operator form:

$$\partial_t H_1(x, y, t) = \mathcal{L}H_1(x, y, t) + a_1. \tag{12}$$

 $H_1(x, y, t)$ is written in a separable form:

$$H_1(x, y, t) = T(t)R(x, y)$$

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and substitution of this into the homogeneous form of Equation (12) yields:

$$\frac{T(t)}{T(t)} = \frac{\mathcal{L}R(x,y)}{R(x,y)} = \lambda$$

where λ is an eigenvalue. The spatial equation is:

$$\mathcal{L}R(x,y) - \lambda R(x,y) = 0, \qquad (13)$$

which has eigenvalue solutions $\mathcal{E}(x, y)$.

Now, in general it cannot be assumed that the eigenfunctions are orthogonal, and it is also convenient simply to consider eigenfunction expansions truncated after M terms, and to consider the eigenfunctions evaluated at M points; this is what emerges from solving the algebraic eigenvalue problem resulting from the discretization of the operator \mathcal{L} , which is denoted by the matrix **F**. Suppose that R(x, y)is represented by M points sampled on the grid; these points have value r_{ℓ} , $\ell = (1, M)$. Then, the matrix representation of Equation (13) is:

$$\mathbf{Fr} - \mathbf{\Lambda r} = \mathbf{0}$$

where the diagonal entries of the matrix Λ are the eigenvalues. This is an algebraic eigenvalue problem (Wilkinson, 1965), which is satisfied by M linearly independent eigenvectors. We construct a matrix \mathbf{E} the *i*th column of which is the *i*th eigenvector evaluated at M points. Thus, *i* is an index of spatial mode number.

It will be assumed that these eigenfunctions are linearly independent and form a complete set — there have been no cases found where this is not true. It may thus be written that:

$$H_1 = \sum_{i=1}^{\infty} T_i(t) E_i(x, y), a_1 = \sum_{i=1}^{\infty} T_i(t) a_i(x, y)$$

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and, after using Equation (13) the perturbation Equation (12) becomes:

$$\sum_{i} \dot{T}_i \mathcal{E}_i = \sum_{i} \lambda_i T_i \mathcal{E}_i + a, (x, y) \in [-1, 1]^2.$$
(14)

By sampling Equation (14) at M points, this equation may be written as a discretized matrix equation:

$$\mathbf{E}\dot{\mathbf{T}} = \mathbf{E}\mathbf{A}\mathbf{T} + \mathbf{a} \tag{15}$$

where **a** is the vector of accumulation rate sampled at the M points. There are thus M linear equations corresponding to the M points of evaluation, and the elevations at the sampling points are given by:

$\mathbf{h} = \mathbf{ET},$

where **h** is the vector of $H_{1,\ell}$ at the sampling points. By multiplying Equation (15) by \mathbf{E}^{-1} , the existence of which is assured by the fact that the eigenvectors are independent, Mmode-evolution equations are obtained:

$$\dot{\mathbf{T}} = \mathbf{\Lambda}\mathbf{T} + \mathbf{E}^{-1}\mathbf{a} \tag{16}$$

with the *rows* of the inverse eigenvector matrix playing the role of a modal weighting function in space for the accumulation rate. By definition $\mathbf{F} = \mathbf{E} \mathbf{\Lambda} \mathbf{E}^{-1}$.

At steady state, we have $\mathbf{EAT} = -\mathbf{a}$, whence

$$\mathbf{h} \equiv \mathbf{E} \ \mathbf{T} = \mathbf{E} \mathbf{\Lambda}^{-1} \mathbf{E}^{-1} \mathbf{a} = \mathbf{G} \mathbf{a} \tag{17}$$

where $\mathbf{G} = -\mathbf{F}^{-1}$ plays a role analogous to a Green's function. A refinement is to suppose that N modes have sufficiently slow relaxation (small eigenvalues) that it is necessary to consider their dynamic values, while the remaining L = M - N modes are regarded as being in steady state. Then, a quantity $\mathbf{h}_{\rm L}$ can be constructed which represents that part of the perturbation that relaxes sufficiently quickly to be in equilibrium with the instantaneous forcing. These are the so-called "slaved" modes, which are computed according to:

$$\mathbf{h}_{\mathrm{L}} = \mathbf{G}_{\mathrm{L}} \mathbf{a},\tag{18a}$$

$$\mathbf{G}_{L} = \mathbf{E}_{:,(N+1):M} \mathbf{\Lambda}_{(N+1):M,(N+1):M}^{-1} \mathbf{E}_{(N+1):M,:}^{-1}$$
(18b)

where colon ("Matlab") notation is used in the subscripts (Golub and Van Loan, 1989, p. 7). For example, the range of indices being considered are represented by a : b, with a single colon by convention representing the total range.

Here, \mathbf{G}_{L} can be regarded as the Green's function for the slaved modes. The evolution of the remaining N dynamic modes is given by

$$\mathbf{\hat{T}}_{1:N} = \mathbf{\Lambda}_{1:N,1:N} \mathbf{T}_{1:N} + \mathbf{E}_{1:N,:}^{-1} \mathbf{a}$$
(19)

so that:

$$\mathbf{h} = \mathbf{h}_{L} + \mathbf{E}_{:,1:N} \mathbf{T}_{1:N}.$$

In practice, one often does not wish to compute the whole eigenvalue sequence, and it is a straightforward exercise to show that:

$$\mathbf{G}_{\mathrm{L}} = \mathbf{G} - \mathbf{E}_{:,1:\mathrm{N}} \mathbf{\Lambda}_{::\mathrm{N},1:\mathrm{N}}^{-1} \mathbf{E}_{1:\mathrm{N},:}^{-1}$$
(20)

Thus, it is necessary to compute \mathbf{G} , the matrix inverse of the operator matrix \mathbf{F} , and those eigenvalues that relax sufficiently slowly that we are interested in their dynamics. Truncations of such generalised Fourier expansions of ice sheets have been considered by Hindmarsh (1990), who concluded that computation of the evolution of a few dynamic modes represented the evolution of the ice sheet reasonably well.

In IHD the first-order perturbation Equations (10) and (11) can be written in Sturm–Liouville form and solved using either finite-difference methods or shooting methods (Hindmarsh, in press). The eigenfunctions are orthogonal. In 2HD, this is not true in general and the perturbation equation, which includes cross-derivative terms, is discretized using a standard nine-point conservative stencil, which produces a sparse, non-symmetric matrix. The eigenvalue problem was solved using the ARPACK software (Sorensen, 1992) which deals specifically with large, sparse, non-symmetric problems. The software uses Arnoldi iteration (see e.g. Chatclin, 1993), producing the "Ritz values", which are approximations to the eigenvalues.

TEST: PERTURBATION TO THE EISMINT BENCH-MARK

The Eismint Benchmarks (EBs) (Huybrechts and others, 1996) are a set of benchmark experiments designed for the purpose of model evaluation. The isothermal VN benchmark, where uniform accumulation is prescribed on a square domain with VN margins (i.e. zero thickness and finite flux of ice) are not considered here. It will be considered in the scaled domain $(x, y) \in [-1, 1] \times [-1, 1]$ with unit accumulation and rate factor C. In this case, the zeroth order solution is computed and is shown in Figure 1a. The zeroth order fluxes are shown in Figure 1b. The results are in a dimensionless system, the details of which are unimportant as relative errors between linear and non-linear computations are considered.

Some modes for the perturbation around the Eismint benchmark are shown in Figure 2. Two of these are volumetric modes, while activation of the other two does not result in volume changes but does produce asymmetry in the ice sheets. Corresponding accumulation sampling functions are shown in Figure 3. These show broadly similar patterns, necessarily to the extent that the symmetries between modes and sampling functions are the same, but there are differences in detail between the eigenfunctions and the



Fig. 1. The EB experiment (Huybrechts and others, 1996). (a) The steady-state elevation in scaled units. (b) Absolute dimensionless flux. (c) In-phase component of elevation for 20 ka forcing; note reverse axis. (d) Out-of-phase component of elevation for 20 ka forcing.

sampling functions. For example, activation of the slowest mode requires a proportionately greater amount of accumulation nearer the centre; this feature also occurs in lHD (Hindmarsh, in press).

The scaling relation (e.g. Hindmarsh, 1990) shows the response of the ice-sheet thickness to changes in the accumulation rate is $H_0 \sim a_0^{1/(m+\nu)}$. The fact that the accumulation rate is uniform implies that the normalized elevation of the ice-sheet (i.e. normalized by the maximum elevation) is unchanged under uniform changes in accumulation, while the maximum elevation behaves according to this scaling rule. We can linearize the scale rule:

$$\frac{\mathrm{d}H_0}{\mathrm{d}a_0} = \frac{1}{m+\nu} \frac{H_0}{a_0}$$

and this is the behaviour that should be followed by the lincarized model: a uniform change in accumulation will lead to a uniform relative change in elevation according to this formula.

Calculations with the discretized operator **G** show that this behaviour is obtained to round off error for a selection of m and ν . It did not matter whether the zeroth-order solution was computed using finite-difference techniques or was an analytical solution, obtainable for the cases $(m, \nu) = (0, 1), (3, 1)$ (Hindmarsh and Payne, 1996). This is because it has been ensured that the zeroth-order solution respects continuity "exactly" (i.e. to round off error).

A more complicated case is periodic forcing of the accumulation rate. Consider a system forced at several frequencies k = (1, K)

$$\dot{T}_i = \lambda_i T_i + \sum f_{ik} \cos(\omega_k t + \chi_k)$$

which has standard solution

$$T_i = A_{ik} \cos(\omega_k t + \phi_{ik} + \chi_k), \qquad (21a)$$

$$\operatorname{an}\phi_{ik} = \frac{\omega_k}{\lambda_i},\tag{21b}$$

$$A_{ik} = \frac{-\lambda_i f_{ik}}{\cos \phi_{ik} (\lambda_i^2 + \omega_k^2)} = \frac{\omega_i f_{ik}}{\sin \phi_{ik} (\lambda_i^2 + \omega_k^2)}.$$
 (21c)

Here,

t

$$f_{ik} = \int \mathcal{E}_i^* \bar{a}_{\ell k}(x, y) \mathrm{d}S$$

or in matrix notation: $\mathbf{f}_i = \mathbf{E}_i^{-1} \bar{a}_k,$

where $\bar{a}_{\ell k}$ represents the pointwise Fourier transform of the accumulation distribution in time. In practice, this formalism is overcomplicated because there is insufficient data, and the accumulation might be specified as varying uniformly in space according to a few selected frequencies.

From the point of view of comparing results, it is more convenient to carry out a spectral analysis of the results of the EB, and compare these with the analytical solution presented above. The elevation at each interior point of the EB grid forms a time series the periodogram of which can be formed (the data are so clean that periodograms suffice). Since the Eismint experiments are forced at one period only, only the amplitude and phase information need to be retrieved at the appropriate frequency. In practice, power might be expected at harmonic frequencies owing to nonlinear effects ("beats"), but these will be ignored in the following analysis. The error this introduces is not great.

Thus, for each point of the EB grid, at the fundamental frequency (the frequency of forcing), the spatial variation of the Fourier components is considered. More specifically, denote by $\bar{s}_{\ell k}$ the discrete Fourier transform of the elevation of the points (x_{ℓ}, y_{ℓ}) at a frequency ω_k (a more intuitive description is provided below). For example, Figure 1c and d



Fig. 2. Eigenfunctions of the EB. Four modes are illustrated; the two lefthand ones are volumetric, while excitation of the two righthand ones results in asymmetry. E number is the mode number.



Fig. 3. Accumulation-rate distribution which excites the corresponding mode number. This is computed by inverting the eigenfunction matrix.

shows the real and imaginary components of $\bar{s}_{\ell k}$ at the forcing period (in this case 20 ka). Table 2 shows the amplitude of the Fourier transform of the centre-point elevation at selected multiples of the forcing frequency. The amplitude of the second harmonic is at most 15% of the first harmonic.

Then, for a given frequency ω_k the Fourier coefficients can be projected onto the discretized eigenvectors **E** thus:

$$\mathbf{c}_k = \mathbf{E}^{-1} \mathbf{\overline{s}}_k,$$

where $\overline{\mathbf{s}}_k$ is the vector formed from $\overline{s}_{\ell k}$ and c_k , formed from c_{ik} , is a vector of mode coefficients corresponding to the frequency k. Amplitude $|c_k|$ and phase information $\phi_k = \arg c_k$ for each mode *i* can be computed and compared with the analytical solution. In practice, this is only applied at the driving frequency.

It is helpful to consider this visually. The steady-state EB profile (Fig. 1a) is subjected to a periodic forcing. The point

Table 2. The Fourier transformation of the centre elevation in the EB for forcings of 20 and 40 ka. Amplitudes for the first four harmonics are given, showing that non-linear behaviour accounts for between 10 and 14% of the signal

Forcing period	Harmonic	Amplitude	
а			
20 000	1	1.1×10^{-1}	
	2	1.2×10^{-2}	
	3	1.8×10^{-3}	
	4	3.9×10^{-1}	
40 000	1	1.2×10^{-1}	
	2	1.8×10^{-2}	
	3	3.4×10^{-5}	
	4	7.8×10^{-1}	

elevations are Fourier-transformed to yield the surfaces shown in Figure lc and d; these are the coefficients $\bar{s}_{\ell k}$. These surfaces can be represented, quite efficiently, as a series of the eigenfunctions from the linearization and shown in Figure 2. The coefficients \mathbf{c}_k multiplying the eigenfunctions in this series are obtained by computing the inner product of the surfaces in Figure lc and d (the Fourier coefficients of the forcing of the Eismint experiment) with the sampling functions shown in Figure 3.

The accumulation-rate variation specified in the EB is large $(a = 0.3 \pm 0.2 \text{ m a}^{-1})$ but the maximum error in the *perturbation* which is associated with oscillation of the first (slowest) mode is 7%. This can be seen from Table 1, which lists the components c_{ik} . (Several have been omitted because symmetry enforces c_{ik} to be zero for uniform accumulation). For forcing at 40 000 years, the error in the computed amplitude for the first few non-zero modes reaches 10% but the dominating contribution comes from the first mode where the error is 6%. Phase lags are around $\pi/2$ for both models. For forcing at 20 000 years, where the amplitude deviation is smaller, the accuracy is higher. On to these errors should be added the errors arising from ignoring the higher harmonics, making the total error about 20%.

These errors are not negligible but the EB is a fairly severe test with accumulation amplitude two-thirds of the mean accumulation, somewhat larger than those experienced during the Ice Age by either the Antarctic or the Greenland ice sheets. The smaller perturbation associated with the shorter period forcing has a smaller error.

NORMAL-MODE ANALYSIS OF SOME ANTARCTIC DEMs

Two Antarctic digital elevation models (DEM), both with 80 km grids (Budd and Smith, 1982, 1985; Bamber and Huy-

brechts, 1996) with associated grids of basal elevation and surface accumulation rate were used. Balance fluxes were calculated and the normal modes computed. These coarse grids were used because it is still a formidable computational task to compute all the modes for finer grids, and it seemed desirable to compute all the modes in smaller test cases rather than truncating arbitrarily with finer grids. The Bamber and Huybrechts (1996) elevation grid is more accurate than the Budd and Smith (1985) grid, but there is an issue of the sensitivity of the slower modes to data uncertainty. In both computations the accumulation data from Budd and Smith (1985) are used. Hindmarsh (in press) has discussed the robustness of one-dimensional (1-D) perturbations to the ice-sheet equation. In this case, a Sturm-Liouville equation is obtained and the robustness of their spectra to model (not solution) perturbation is well understood (Pryce, 1993). While Sturm-Liouville forms cannot be obtained in higher dimensions, the robustness property is expected to be maintained.

Balance fluxes and normal modes were computed in the manner described above using $\nu = 3, m = 5$, corresponding to internal deformation according to a Glen (1955) rheology. A puzzling feature was the presence of eigenvalues and vectors with non-zero imaginary parts. The non-zero parts of the eigenvalues were at most no more than a few per cent of the corresponding real parts. There are several possible causes for this but, if one considers the ice-sheet equation in the 1-D form

$$\partial_t H = \partial_x \left(C(s-b)^m |\partial_x s|^{\nu-1} \partial_x s \right) + a,$$

and expands:

$$\partial_t H = C(s-b)^m \partial_x \Big(|\partial_x s|^{\nu-1} \partial_x s \Big) + \\ m \Big(|\partial_x s|^{\nu-1} \partial_x s \Big) \Big(C(s-b)^{m-1} \Big) (\partial_x s - \partial_x b) + a,$$

then, if $|\partial_x b| \gg |\partial_x s|$,

$$\partial_t H = -m \Big(|\partial_x s|^{\nu-1} \partial_x s \Big) \Big(C(s-b)^{m-1} \Big) \partial_x b + a,$$

which is a first-order hyperbolic equation. In such a case, one is less surprised to see complex eigenvalues and they may therefore arise from rugose basal topography. The argument of the eigenvalues (i.e. $Im(\lambda)/Re(\lambda)$) is plotted in Figure 4. Complex eigenvectors only occur when complex eigenvalues exist. Figure 4 shows that this problem only exists for higher-mode numbers. The following discussion refers to the real parts of the modes.

The six slowest modes for each case are shown in Figures 5 and 6, together with associated time constants and volumes relative to the slowest mode. The results are broadly similar and the percentage differences between the computed time constants are smaller than the uncertainty in the rheological indices ν and m.

A significant result is that these low-order modes are smooth, despite the use of accurate data in the MSSL dataset. Thus, the process of computing the normal modes in effect filters the data in the sense that small-scale spatial variation is only excited by small-scale forcing.

These modes are clearly East Antarctic modes and relate to the fact that the time constants for East Antarctica are greater than for West Antarctica owing to the low accumulation rates (e.g. Hindmarsh, 1990). Evidently, the Lambert Basin splits the glaciodynamic response of East Antarctica asunder. The temptation should be resisted to



Fig. 4. The argument of the eigenvalue plotted against mode number. Non-zero arguments are a numerical artefact. They do not appear in modes of < order 100.

conclude that coarse grids are sufficient to compute the normal modes of an ice sheet. The analysis of Budd and Warner (1996) shows how flow is directed into streams and it can be seen from the perturbation Equation (11) that spatial variations in the zeroth-order discharge might well have a significant effect.

The accumulation-rate sampling distributions (i.e. the rows of \mathbf{E}^{-1}) are shown in Figure 7. Their spatial structure is broadly similar to the modes, as is the case in lHD (Hindmarsh, in press), but owing to their non-orthogonality, do not excite only the corresponding mode, as compared to the orthogonal functions that appear in lHD.

Volumetric spectra (i.e. the eigenfunction volume plotted against its associated time constants) are shown in Figure 8. The slowest modes have time-steps of around 10 000 years, which can be predicted from the scale relationship H/a(2n + 2). The volumetric spectrum indicates the relaxation time-scales of volumetric significance. The modes with short time constants do, in sum of absolute magnitude, represent a considerable volume but these modes are associated with spatial length scales smaller than likely variation in the accumulation rate and will not therefore be activated significantly. Thus, most of the volumetric response

Table 3. The amplitudes of some spatial modes in the EB configuration for forcings of period 20 and 40 ka, compared with the linear solutions. The linear amplitudes depend on the forcing period but the effect is too small to be seen at the quoted accuracy

Forcing period	Mode number	Mode amplitude for linear solution	Linear amplitude EB amplitude
а			
20 000	1	2.3	1.0
	6	0.28	0.93
	13	0.099	1.06
	17	0.089	0.92
40 000	I	2.3	0.93
	2	0.28	0.90
	3	0.099	0.96
	4	0.089	0.90



Fig. 5. Six slowest modes computed from the MSSL dataset (Bamber and Huybrechts, 1996). Associated time constants and relative volumes are indicated. Contour interval 0.2; black and white contours are of opposite sign.

seems to be concentrated between 1000 and 10 000 years. This is consistent with conclusions obtained by Huybrechts (1992) using a non-linear thermomechanically coupled model.

It is possible, using the procedure described in Equations (18) to (20), to compute the response of the ice sheet to changes in the accumulation rate. The eigenfunctions can

be used to decompose the spatial distribution of the accumulation and the evolution split between fast, slaved modes (with high wave-number spatial variability) the instantaneous contribution of which is described by Equation (18a) and the slow, large spatial-scale modes the evolution of which is described by the dynamical Equation (19). In this



Fig. 6. Six slowest modes computed from the UM dataset (Budd and others, 1982). Associated time constants and relative volumes are indicated. Contour interval 0.2; black and white contours are of opposite sign.



Fig. 7. Distribution of accumulation that optimally excites the corresponding mode, MSSL dataset. These accumulation distributions will excite other modes as they are not orthogonal. Contour interval 0.2; black and white contours are of opposite sign.



Fig. 8. Volumetric spectrum: mode volume plotted against the associated time constant. MSSL data plotted in heavy line, UM dataset in dotted line.

way, the spatial structure associated with the fast modes can be retained in the evolution calculation. In non-linear models, data inconsistencies associated with the fast modes tend to cause numerical problems (e.g. Oerlemans and Van der Veen, 1984) and data inconsistencies are relaxed out by running the model. Space limitations preclude further discussion of this important application.

CONCLUSIONS

Of the three options discussed for initialization, the easiest one, which uses observed elevations in the zeroth-order solution, seems to be a feasible way of initializing models.

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This is because the smaller-scale structure in the zerothorder solutions is not manifested in the low-order modes of the perturbed solution. The practical consequence of this is high accuracy. Normal-mode analyses permit small spatial structure to be retained in models without being relaxed out, where it is due to data inconsistency or causing numerical instability. There remains a problem of how to deal with sink holes.

The normal modes of two Antarctic DEMs have been computed. The differences in elevation cause relatively small variations in the spectrum and the qualitative features of the eigenfunctions remain similar for slower modes. The *e*-folding relaxation time constant for East Antarctica is around 10 000 years. The volumetric aspect of the relaxation of Antarctica has been computed, with the most significant response occurring on time-scales between 1000 and 10 000 years. What causes the spatial structure of the modes is not obvious and requires further investigation. Better physics, in particular the representation of grounding-line motion and of sliding, should be available in the future.

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